

RHEOLOGICAL EQUATIONS OF STATE FOR WEAK SOLUTIONS OF POLYMERS WITH RIGID ELLIPSOIDAL MACROMOLECULES

P. B. Begoulev and Yu. I. Shmakov

UDC 532.135:541.182.6

Based on the structural-continuum model, the rheological equations of state are derived for weak solutions of polymers with rigid macromolecules in the shape of triaxial ellipsoids.

The rheological equations of state have been derived in [1, 2], from different viewpoints, for weak solutions of polymers with a rigid ellipsoid of revolution serving as the hypothetical model of the macromolecules. From the structural-continuum viewpoint [1], we will now consider the case where the hydrodynamic model of the polymer macromolecules in solution is a rigid triaxial ellipsoid.

We will use the structural-continuum model [3] for describing the rheological behavior of such a medium. A feature of structural-continuum models is the revised concept of the continuum point, with every point here characterizable not only by the density but also by the rate of change of several inner parameters. We will consider the flow of a structural continuum relative to a stationary Cartesian system of coordinates x^i ($i = 1, 2, 3$). Assuming that the stress tensor t_{ij} depends on the shear-rate tensor d_{ij} and on two inner parameters, namely the inertia tensor I_{ij} and the angular-velocity tensor Ω_{ij} , we obtain, when t_{ij} is a linear function of d_{ij} and $V_{ij} = \omega_{ij} - \Omega_{ij}$, the following expression for the symmetric part $t_{(ij)}$ and for the asymmetric part $t_{[ij]}$ of the stress tensor:

$$t_{(ij)} = -p\delta_{ij} + \alpha_1 I_{ij} + \alpha_2 d_{ij} + \alpha_3 I_{ij}^2 + \alpha_4 (I_{ik} d_{kj} + d_{ik} I_{kj}) + \alpha_5 (I_{ik} V_{kj} - V_{ik} I_{kj}) + \alpha_6 (d_{ik} I_{kj}^2 + I_{ik}^2 d_{kj}) + \alpha_7 (V_{ik} I_{kj}^2 - I_{ik}^2 V_{kj}) + \alpha_8 (I_{ik} V_{km} I_{mj}^2 - I_{ik}^2 V_{km} I_{mj}), \quad (1)$$

$$t_{[ij]} = \beta_1 V_{ij} + \beta_2 (I_{ik} d_{kj} - d_{ik} I_{kj}) + \beta_3 (V_{ik} I_{kj} + I_{ik} V_{kj}) + \beta_4 (V_{ik} I_{kj}^2 + I_{ik}^2 V_{kj}) + \beta_5 (d_{ik} I_{kj}^2 - I_{ik}^2 d_{kj}) + \beta_6 (I_{ik} d_{km} I_{mj}^2 - I_{ik}^2 d_{km} I_{mj}), \quad (2)$$

where α_i ($i = 1, 2, \dots, 8$) and β_k ($k = 1, 2, \dots, 6$) are polynomial functions of the first tensor invariants I_{ij} , I_{ij}^2 , I_{ik}^3 , $I_{ik} d_{kj}$, $d_{ik} I_{kj}^2$, which do not violate the linearity of the t_{ij} dependence on d_{ij} and V_{ij} . Inasmuch as the structural-continuum model (1), (2) is used in setting up the rheological equations of state for solutions of polymers with rigid ellipsoidal macromolecules, we relate the inner parameters I_{ij} and Ω_{ij} in (1) and (2) to the respective characteristics of ellipsoidal macromolecules.

Let $\vec{n}_1, \vec{n}_2, \vec{n}_3$ be mutually orthogonal unit vectors defining the orientation of an ellipsoidal macromolecule along axes a, b, c , respectively, then I_{ij} can be represented as

$$I_{ij} = I_1 n_i n_j + I_2 n_i^2 n_j^2 + I_3 n_i^3 n_j^3. \quad (3)$$

We will disregard the inner moment of momentum, which makes $t_{[ij]} = 0$ [4], and then, with the aid of (2) and (3), we obtain for the angular-velocity tensor Ω_{ij}

$$\Omega_{ij} = \alpha_{m k m k} d_{si} n_s n_i n_j n_j - \omega_{ij}, \quad (4)$$

T. G. Shevchenko State University, Kiev. Translated from *Inzhenerno-Fizicheski Zhurnal*, Vol. 23, No. 2, pp. 340-344, August, 1972. Original article submitted November 28, 1971.

© 1974 Consultants Bureau, a division of Plenum Publishing Corporation, 227 West 17th Street, New York, N. Y. 10011. No part of this publication may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, microfilming, recording or otherwise, without written permission of the publisher. A copy of this article is available from the publisher for \$15.00.

where $\alpha_{mk} = -\alpha_{km}$ are functions of β_k ($k = 1, 2, \dots, 6$) and I_1, I_2, I_3 . Inserting (3) and (4) into (1), with the mutual orthogonality of unit vectors $\overset{i}{n}$ taken into consideration, we represent the stress tensor as

$$t_{ij} = -p\delta_{ij} + 2\mu_1 d_{ij} + \mu_2 d_{km} \overset{1}{n}_k \overset{1}{n}_m \overset{1}{n}_i \overset{1}{n}_j + \mu_3 d_{km} \overset{2}{n}_k \overset{2}{n}_m \overset{2}{n}_i \overset{2}{n}_j + \mu_4 d_{km} \overset{2}{n}_k \overset{1}{n}_m \overset{1}{n}_i \overset{2}{n}_j + \mu_5 \overset{1}{n}_i \overset{1}{n}_j + \mu_6 \overset{2}{n}_i \overset{2}{n}_j + \gamma_{km} d_{st} \overset{k}{n}_s \overset{m}{n}_t \overset{k}{n}_i \overset{m}{n}_j, \quad (5)$$

where $\nu_{km} = \nu_{mk}$ ($k, m = 1, 2, 3, k \neq m$).

In order to determine the rheological constants in (5), we make use of the stress tensor σ_{ij} , which applies to our medium in a moving system of coordinates $\overset{i}{n}$ and which is related to the ellipsoid as follows [5]:

$$\sigma_{ij} = -p\delta_{ij} + 2\mu d_{ij} + \frac{8\mu\Phi}{abc} A_{ij}, \quad (6)$$

where

$$A_{ij} = \begin{pmatrix} \frac{2\alpha_0'' d_{11} - \beta_0'' d_{22} - \nu_0'' d_{33}}{6F}, & \frac{d_{12}}{2\nu_0'(a^2 + b^2)}, & \frac{d_{13}}{2\beta_0'(c^2 + a^2)} \\ \frac{d_{12}}{2\nu_0'(a^2 + b^2)}, & \frac{2\beta_0'' d_{22} - \nu_0'' d_{33} - \alpha_0'' d_{11}}{6F}, & \frac{d_{23}}{2\alpha_0'(b^2 + c^2)} \\ \frac{d_{13}}{2\beta_0'(c^2 + a^2)}, & \frac{d_{23}}{2\alpha_0'(b^2 + c^2)}, & \frac{2\nu_0'' d_{33} - \alpha_0'' d_{11} - \beta_0'' d_{22}}{6F} \end{pmatrix},$$

$F = (\alpha_0'' \beta_0'' + \alpha_0'' \nu_0'' + \beta_0'' \nu_0'')$, $\alpha_0, \beta_0, \nu_0, \alpha_0', \beta_0', \nu_0', \alpha_0'', \beta_0'', \nu_0''$ are functions of a, b, c [6]. Transformation of Eq. (5) to the moving system of coordinates $\overset{1}{n}(1, 0, 0)$, $\overset{2}{n}(0, 1, 0)$, $\overset{3}{n}(0, 0, 1)$ and comparison with (6) will yield the following expressions for the rheological constants:

$$\mu_1 = \mu \left(1 + \frac{2\Phi}{abc} \cdot \frac{\nu_0''}{F} \right), \quad (7)$$

$$\mu_2 = \frac{4\mu\Phi}{abc} \cdot \frac{\alpha_0'' - \nu_0''}{F}, \quad (8)$$

$$\mu_3 = \frac{4\mu\Phi}{abc} \cdot \frac{\beta_0'' - \nu_0''}{F}, \quad (9)$$

$$\mu_4 = 0, \quad (10)$$

$$\nu_{12} = \frac{4\mu\Phi}{abc} \left(\frac{1}{\nu_0'(a^2 + b^2)} - \frac{\nu_0''}{F} \right), \quad (11)$$

$$\nu_{13} = \frac{4\mu\Phi}{abc} \left(\frac{1}{\beta_0'(a^2 + c^2)} - \frac{\nu_0''}{F} \right), \quad (12)$$

$$\nu_{23} = \frac{4\mu\Phi}{abc} \left(\frac{1}{\alpha_0'(b^2 + c^2)} - \frac{\nu_0''}{F} \right). \quad (13)$$

Based on a comparison of (5) and (6), we ought to let $\mu_5 = \mu_6 = 0$, but the terms $\mu_5 \overset{1}{n}_i \overset{1}{n}_j$, $\mu_6 \overset{2}{n}_i \overset{2}{n}_j$, as well as $\mu_1 \overset{1}{n}_i \overset{1}{n}_j$ in the case of an ellipsoid of revolution in [1] may represent stresses due to rotational Brownian movement not accounted for in [5]. Leaving μ_5 and μ_6 undetermined as yet, we will consider the expression (5) averaged through the distribution function in [7], which characterizes the orientation of an ellipsoidal macromolecule due to hydrodynamic forces and rotational Brownian movement,

$$\langle t_{ij} \rangle = -p\delta_{ij} + 2\mu_1 d_{ij} + \mu_2 d_{km} \langle \overset{1}{n}_k \overset{1}{n}_m \overset{1}{n}_i \overset{1}{n}_j \rangle + \mu_3 d_{km} \langle \overset{2}{n}_k \overset{2}{n}_m \overset{2}{n}_i \overset{2}{n}_j \rangle + \mu_5 \langle \overset{1}{n}_i \overset{1}{n}_j \rangle + \mu_6 \langle \overset{2}{n}_i \overset{2}{n}_j \rangle + \nu_{km} d_{st} \langle \overset{k}{n}_s \overset{m}{n}_t \overset{k}{n}_i \overset{m}{n}_j \rangle, \quad (14)$$

is the rheological equation of state for our medium, where μ_1, μ_2, μ_3 , and ν_{km} are defined by Eqs. (7)-(13), respectively.

In order to determine the rheological constants μ_5 and μ_6 , we will find the dissipation of mechanical energy S in a simple shear flow:

$$v_i = G_{ij} \dot{x}_j, \quad G_{ij} = \begin{vmatrix} 0 & 0 & 0 \\ K & 0 & 0 \\ 0 & 0 & 0 \end{vmatrix}, \quad (15)$$

due to the occurrence of rotational Brownian movement.

According to [8], this component of mechanical energy dissipation is

$$S = \frac{4\mu\Phi K}{abc} \left\langle \left[\frac{(c^2 - b^2) h_{32} - (c^2 + b^2) o_{32}}{b^2\beta_0 + c^2\nu_0} W_1 + \frac{(b^2 - a^2) h_{21} - (b^2 + a^2) o_{21}}{a^2\alpha_0 + b^2\beta_0} W_3 + \frac{(a^2 - c^2) h_{13} - (a^2 + c^2) o_{13}}{a^2\alpha_0 + c^2\nu_0} W_2 \right] \right\rangle, \quad (16)$$

where

$$\|h_{ij}\| = \frac{1}{2} (A^{-1}GA) + \frac{1}{2} (A^{-1}GA)',$$

$$\|o_{ij}\| = \frac{1}{2} (A^{-1}GA) - \frac{1}{2} (A^{-1}GA)',$$

Here A is the transformation matrix from the moving system of coordinates $\overset{i}{n}$ to the stationary system of coordinates $\overset{i}{x}$, the prime sign denoting a transformation. After performing several operations, we can write relation (16) as

$$S = \frac{\mu\Phi K}{abc} \left[\frac{D_r^2(a^2 - c^2)}{c^2\nu_0 + a^2\alpha_0} (8 \langle \overset{1}{n}_1 \overset{1}{n}_2 \rangle + 4 \langle \overset{2}{n}_1 \overset{2}{n}_2 \rangle) + \frac{D_r^3(a^2 - b^2)}{a^2\alpha_0 + b^2\beta_0} (4 \langle \overset{1}{n}_1 \overset{1}{n}_2 \rangle - 4 \langle \overset{2}{n}_1 \overset{2}{n}_2 \rangle) + \frac{D_r^1(b^2 - c^2)}{b^2\beta_0 + c^2\nu_0} (8 \langle \overset{2}{n}_1 \overset{2}{n}_2 \rangle + 4 \langle \overset{1}{n}_1 \overset{1}{n}_2 \rangle) \right]. \quad (17)$$

It follows from (17) that the terms $\mu_5 \langle \overset{1}{n}_1 \overset{1}{n}_2 \rangle$, $\mu_6 \langle \overset{2}{n}_1 \overset{2}{n}_2 \rangle$ in (14) are indeed stresses due to rotational Brownian movement and that μ_5 , μ_6 are, respectively:

$$\mu_5 = \frac{\mu\Phi}{abc} \left[8 \frac{D_r^2(a^2 - c^2)}{a^2\alpha_0 + c^2\nu_0} + 4 \frac{D_r^3(a^2 - b^2)}{a^2\alpha_0 + b^2\beta_0} + 4 \frac{D_r^1(b^2 - c^2)}{b^2\beta_0 + c^2\nu_0} \right], \quad (18)$$

$$\mu_6 = \frac{\mu\Phi}{abc} \left[4 \frac{D_r^2(a^2 - c^2)}{a^2\alpha_0 + c^2\nu_0} + 4 \frac{D_r^3(b^2 - a^2)}{a^2\alpha_0 + b^2\beta_0} + 8 \frac{D_r^1(b^2 - c^2)}{b^2\beta_0 + c^2\nu_0} \right]. \quad (19)$$

In the special case where $b = c$, the rheological equations of state (14) become the earlier derived equations of state [1] for weak solutions of polymer macromolecules with a rigid ellipsoid of revolution as the hypothetical hydrodynamic model. When $a = b = c$, Eqs. (14) yield Einstein's classical result [9].

NOTATION

t_{ij}	is the stress tensor;
p	is the isotropic pressure;
δ_{ij}	is the Kronecker delta;
d_{ij}	is the strain-state tensor;
ω_{ij}	is the velocity-vortex tensor;
Ω_{ij}	is the inner parameter: angular-velocity tensor;
I_{ij}	is the inner parameter: inertia tensor;
$\overset{i}{x}$	is the stationary Cartesian system of coordinates;
a, b, c	are the semiaxes of an ellipsoid;
$\overset{i}{n}$	are the unit vectors oriented along the ellipsoid semiaxes a, b, c , respectively;

μ_i, ν_{km}	are the rheological constants;
μ	is the dynamic viscosity of the solvent;
ϕ	is the volume concentration of macromolecules in the solution;
D_i^j	is the rotational diffusivities of the ellipsoid;
$\langle \rangle$	is the symbol of averaging;
$\alpha_0, \beta_0, \nu_0, \alpha_0', \beta_0',$ $\nu_0', \alpha_0'', \beta_0'', \nu_0''$	are the functions of a, b, c according to the Jeffery theory;
S	is the dissipation of mechanical energy, per unit volume, due to rotational Brownian movement;
v_i	are the velocity components in the stationary system of coordinates;
W_i	is the angular velocity of ellipsoid, in the moving system of coordinates, due to rotational Brownian movement.

LITERATURE CITED

1. Yu. I. Shmakov and E. Yu. Taran, *Inzh.-Fiz. Zh.*, 18, 1019 (1970).
2. V. N. Pokrovskii, *Kolloid. Zeitschr.*, 30, 881 (1968).
3. K. A. Kline and S. J. Allen, *Zeitschr. Angew. Matem. und Phys.*, 19, 898 (1968).
4. L. I. Sedov, *Mechanics of Continuous Media [in Russian]*, Vol. 1, Nauka, Moscow (1970).
5. G. L. Hand, *Archiv. Ration. Mech. Analysis*, 7, 81 (1961).
6. J. B. Jeffery, *Proc. Roy. Soc.*, A102, 161 (1922).
7. H. J. Workman and C. A. Hollingsworth, *J. Colloid. Internat. Sci.*, 29, 664 (1969).
8. N. Saito and T. Kato, *J. Phys. Soc. Japan*, 12, 1393 (1957).
9. A. Einstein, *Ann. Physik*, 19, 298 (1906); 34, 591 (1911).